# CHARACTERIZATION OF THERMALLY SPRAYED COATINGS COHESION

F CARASSITI, R. CIGNA, T. VALENTE 2 1 3rd University of Rome, Italy. 2 University of Rome «La Sapienza», Italy.

# 1. INTRODUCTION

The major limitation for the development of cramic coatings and their full application on an industrial scale, as well as expanding their range of applications, lies in their poor fracture toughness. The coating is usually considered to be a homogeneous and monolithic deposit that is constrained and controlled by the engineering properties of the substrate, but in most case, taking into account is tract behaviour, it should be considered as planar oriented composite countries are all the considered as planar oriented composite countries are all the considered as planar oriented composite countries are all the considered as planar oriented composite countries are all the considered as planar oriented composite countries.

Plasma sprayed coatings have been developed and optimized over the last decade. The engineering properties which have been taken advantage include corrosion protection, control of the wear rate and thermal barriers. The main result was an extended life and/or operating limits of the coated component.

Very often the coating is considered as m\*add-on\*, but the present technology of thermal apsysing processes does not permit coatings to be used in application role where the falture leads to the immediate removal of the component from service. Therefore the coating should be considered as one part of the coverall system and the current trend is to design the coating as an integral part of the component assembly under than as an add on to the substrate that the contract of the conformal contract the coating should be contracted as the contract that are an add on to the substrate than as an add on to the substrate than a single contract that a single contract

In effect most costings are well known to be not very reliable. The low reliability means that the material properties of these costings are highly varies ble, due to the lack of enough scientific knowledge of how their microstructure is formed during deposition and to the highly anisotropy of the reading, layer feed structure. Plasma sprayed costings exhibit a lamedlar morphology consisting of fattened "successful-particles." The costings are normally greater than 25 µm in thickness and can thus be described as "sales" and the successful as the likelihoos sand un to 80 µm in diameter.

The lamellar microstructures are complex and they are the result of the deposition and cooling of successive molten droplets where numerous parameters are involved such as temperature of the substrate, spraying atmosphere,

plasma gas properties (velocity, enthalpy), partiele dimensions. The mechanical properties of the contings depend on felects, such as porosity, cracks, lamellae, size, etc. These aspects have a strong influence on the important properties of the deposit such as adhesion between conting and the substrate and cohosion inside the coating. The service failure mode can be described as interfacial, cohosive, or mise dimerfacial cohosion.

## 2. STATE OF THE ART

Many theories and mechanisms have been proposed, none however cover all situations and therefore the best test method is often that which simulates practical stress conditions. Labonatory tests should induce the observed service failures with a scale down criteria as concerns the working time, otherwise such tests will be of limited application to engineering design and quality control.

When critical thermomechanical loading conditions are exceeded, two different patterns of damage can occur:

 a) if the adhesion strength of the coating to the base material is exceeded, the coating peels from the parent body;

b) if the internal coating strength is exceeded, separation occurs within the sprayed coating and the parent body is still covered with coating material in the damaged area.

Cohesive strength is mainly determined by residual stresses, friction and damping inside the compounds. In order to achieve high cohesion, compressive strains inside the coatings should be near the yield limit of compression and particle size should be low.

The yield limit of compression can be tailored by:

 volumetrical stiffness of the substrate length\*width\*heigth\*Young modulus

geometrical stiffness of the substrate
 radii or ring for instance

3. triaxial stress state.

The adhesion of thermally sprayed coatings is not only an interfacial problem of each lamella within a coating, but also involves the integrity of the interface between the substrate and coating, residual stresses, crack population and nore size and distributions.

Different tests methods have been proposed based on macroscopic or microscopic approaches. Two properties are generally distinguished: strength and toughness. Most of measurements are carried out with tenule adhesion tests, to be a second of the design of the design of the design of the design of take into account the difficulty involved with any mechanical property assessment of coating due to the need of attachment of a loading device to the approach. sing without influencing the properties that are being measured. On the microgeogic level the adhesion properties were investigated by shearing individual paridicate from the substrate surface and further theoretical work has treated adhesion as a stochastic process that depends on the formation characteristics of the figure monolayer of material. Assustic emission studies were also proposed in order to assess the crack density function, a product of the number of cracks and crack size.

These methods provide many different approaches to evaluate the adhesion of ex- obseins trength of conting systems. However each this slandarmages and some can clucidate the difference of in service performance. As an example, ten- standard continuation of the difference of proper formance and as continuated to great standard continuation of the standard continuation of the difference of the continuation of the standard and expected specimen preparation, for the standard continuation of the continuation of the other observable of the difference of the continuation of the other observable of the difference of the continuation of the other observable or the other observable of the difference of the other observable or other observable ore

Indentation (eclinique such as micro-Vickers hardness tests have been used to evaluate the fracture toughness of coatings and to demonstrate that the properties of coating are generally anisotropic. These technique, among others, may be used to gain a fundamental understanding of coating performance or quality coerror.

Other tests such as the ACTJP test require a pre-blasted sprayed specimes sented to an angle 9 with a jet stream of alumina particles of suitable weight used as the erosion material to evaluate the resulting weight loss and surface states, jee giving qualitative information on internal strength of the costing. Wear tests — Ogsohi's wear test, ring-on-disk wear and scracks wear — are often out to revolute couring resistance to wear and to obtain inducer information on the contraction of the couring resistance to wear and to obtain inducer information.

# 3. FRETTING WEAR RIG

In order to evaluate the "in service" behaviour of the coating, fretting-corosion tests, a particular class of wear tests, represent an interesting mean of investigation. A dedicated fretting wear rig, schematically shown in fig. 1, was designed together with the Department of Metallurgy and Materials Science of Notringham University.

Tests at high pressure in superheated steam (400°C, 90 bar) and at high temperature (up to 100°C) in air or corrosive atmosphere ( $H_3$ S,  $H_8$ ,  $N_{O_2}$  SO<sub> $O_2$ </sub> SO<sub> $O_3$ </sub> and  $H_3$ ) can be carried out. During the test the applied value of normal load, frequency and amplitude of oscillation can be recorded. After the test the failure morphology can be examined by optical microscopy or SEM.

Preliminary tests were carried out in air at room temperature on piston rings coated with YSZ (yttria-partially stabilized zirconia) subjected to an initial

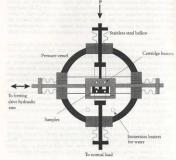


Fig. 1 - Schematic view of the high pressure test facility.

static load that approximately corresponds to the installed bending stress of the ring at nominal diameter and to a dynamic load with an oscillation frequency of 50 Hz. The progressive break-out of the coatings observed during the test in the previous cyclic conditions could be correlated with the coating fracture toughness and with coating porosity and microstructure.

A modified device of measurement has been developed in order to evaluate directly the variation of the friction coefficient during the test. The aim is to assess the progressive coaling scaling off by monitoring the friction coefficient variation, in order to obtain information on coating cobesion properties. This can represent a more powerful information than weight loss and surface morphology after the test and can lead to a correlation with coating hardness, fracture toughness and spraying parameters, because local loads due to friction are responsible of coating scaling off when coating cohesion strength is overcome. Tests are now under development.

A significant result of this kind of test lies in the possibility to reproduce the environmental conditions which characterize the operating environment, so that it must be considered as a complementary method respect to indentation and search tests, more focused on fracture toughness investigation of the as sorrowed continues.

Cohesion properties may be strongly influenced by the corrosion resistance of the conting, and the damages due to those phonomens (e.g. clastiallustino et YSZ due to reactions yrain's S, yrain's V can be responsible for costing failure. The interaction between these different mechanisms needs to be considered in order to achieve a satisfactory costing design, both microstructural and mechanisms of the considered and considere

retaining and application will grow.

A further point to underline is that due to the highly variable nature of the material properties of coatings, statistical analysis of results (i.e. Weibull distribution) is necessary. This requires a suitable number of tests.

## 4. CONCLUSION

The ablesion strength and colesion strength of thermal pure contings on be influenced by many factors, such as spary vailables, proposed characteristics, substrate preparation, post treatments an service conditions. It is very important for materials designers to remember that these properties are strongly related to service conditions and therefore characterization tests which can reproduce real operating conditions are of primary importance. A ferting wear in yas addigned and developed with the aim to reproduce the in-service conditions and no obtain information on the previous properties. Perlimitary tests induces a correlation between coating behaviour and nices barrioless measurements outside on the measurement addres to inserting the better the possible correlation by nonisoring the friction coefficient variation during the test and realize tests at high temperature and high pressure.

WESS L.E., PRINZ F.B., ADAMS D.A., SIEWKORK D.P., J. Therm. Spray Tech., Vol. 1, No. 1 1992. pp. 231-237.

LIN C.K., BERNUT C.C., J. Therm. Spray Tech., Vol. 3, No. 1, 1994, pp. 75-104.

Rives Jones T.N., Surf. Cont. Technol., Vol. 43/44, 1990, pp. 402-415.

MITTAL K.L., Adherion Measurement of Thin Films, Thick Films and Bulk Coatings, STP 640,

K.L. Mittal ed., ASTM, 1978. LYSSIENKO B.A., RISHN V.V., ZIL'SERG V.G., SHARIVKER S. YE., Son Pounder Metall Mo-

Cenaw., Vol 8, 1969, pp. 331-334. ZAMBUROV B.M., TROPINOV M.G., GUSENA L.I., GOLOWON Y.I., KONONOV A.A., VENORUBOVA V.V., Son Pourder Metall. Met. Ceram., Vol. 9, 1970, pp. 925-929.

BIENDY C.C., J. Mater. Erg., Vol. 12, 1990, pp. 151-158.

SHIMEDE Y., SATO M., KORAYASHI M., MAEDA K., Thermal Spray: International Advances in Conting Technology, C.C. Berndt ed., ASM International, 1992, pp. 257-262.

BECHER P.F., NEWELL W.L., HALEN S.A., Fracture Mechanics of Ceramic, Vol. III, R.C. Brade D.P.H. Hasselman, F.F. Lange ed., Plenum Press, 1978, pp. 463-471. Bascon W.D., BITNER J.L., J. Mater., Vol. 2, 1967, pp. 661-681.

DAS D.K., SRIVASTAVA M.P., JOSSE S.V., SIVAKAMUR R., Surf. Coat. Technol., Vol. 46, 1991, pp. 331-345.

SCHBRUTZ C.J., HINTERMAN H.E., Surf. Coat. Technol., Vol. 48, 1991, pp. 1-6 GUIGE M., RICKERRY D.S., KINGSWELL R., SCOTT K.T., Thermal Spray Research and Application

T.F. Bernecki ed., ASM International, USA, 1991, pp. 331-337. MICHIGAN M.M., KRISHCAMINERY R., Thermal Spray: Advances in Coating Technology, C.C.

Berndt, ASM International, 1992, pp. 711-715. IWANOTO N., KAMAI M., UINO G., Thennal Spray, Advances in Coating Technology, C.C. Berndt, ASM International, 1992, pp. 259-265.

LUGSCHEIDER E., JOKEL P., PURSIE G., ROMON O., YUSHGHENKO K., Thermal Spray Advances in Coating Technology, C.C. Berndt, ASM International, 1992, pp. 647-651.

LINEN B.R., MARSITALL D.B., Fracture Mechanics of Geramic, Vol. III, R.C. Bradt, D.P.H. Hasselman, F.F. Lange ed., Plenum Press, 1978, pp. 205-209. FURENCISO K., OKI S., GODHA S., Thermal Spray: Advances in Coating Technology, C.C. Beendt,

ASM International, 1992, pp. 705-709. OSTORIC P., McPriesson R., Mater Forum, Vol. 19, No. 4, 1987, pp. 247-255.

BINNER J.G., STEVENS R., Trans. J. Br. Ceram. Soc., Vol. 83, 1984, pp. 168-172.

RICHARD C., LU J., FLAVENOT J.F., BERANGER G., DECOMPS F., Thermal Spray: Advances in Conting Technology, C.C. Berndt, ASM International, 1992, pp. 11-16.

LIN C.K., BERNDT C.C., Thermal Spray Coatings: Research, Design and Application, C.C. Berndt and T.F. Bernecki ed., ASM International, 1993, pp. 561-568.

CABASSITI F., PROVERMO E., VALENTE T., Proc. SIMCER, Nov. 1992, Rimini.